Agricultural Engineering Research Journal 4 (1): 09-16, 2014 ISSN 2218-3906 © IDOSI Publications, 2014 DOI: 10.5829/idosi.aerj.2014.4.1.1116

Modeling of Radial-Ply Tire Contact Length Based on Overall Unloaded Diameter, Inflation Pressure, Vertical Load and Rotational Speed

Babak Jaberinasab, Majid Rashidi and Iraj Ranjbar

Department of Agricultural Machinery, Takestan Branch, Islamic Azad University, Takestan, Iran

Abstract: This study was conducted to model contact length (L) of radial-ply tire based on overall unloaded diameter (d), inflation pressure (P), vertical load (W) and rotational speed (N). For this reason, contact length of three radial-ply tires with different overall unloaded diameter were measured at three levels of inflation pressure, four levels of vertical load and six levels of rotational speed. In order to model contact length based on overall unloaded diameter, inflation pressure and vertical load, a four-variable linear regression model was suggested and all the data were subjected to regression analysis. The statistical results of study indicated that the four-variable linear regression model L = 552.1 - 0.656 d - 2.930 P + 0.320 W - 0.009 N with R² = 0.9711 may be suggested to predict contact length of radial-ply tire based on overall unloaded diameter, inflation pressure, vertical load and rotational speed for a limited range of radial-ply tire sizes.

Key words: Radial-ply tire • Contact length • Overall unloaded diameter • Inflation pressure • Vertical load • Rotational speed • Modeling

INTRODUCTION

A flexible tire has a smaller contact area on hard surface than it dose on soft ground. A rule of thumb which can be used for estimation of tire contact area is shown by equation 1 [1]:

$$A = bL \tag{1}$$

where:

A = Contact area of tire (m^2) b = Section width of tire (m)L = Contact length of tire (m)

McKyes [1] gave an approximate method for estimating contact length of tire on hard and soft surfaces (Fig. 1) as given below in equations 2 and 3, respectively:

$$L = \frac{d}{4} \text{ (On a hard surface)}$$
(2)
$$L = \frac{d}{2} \text{ (On a soft surface)}$$
(3)

where:

d = Overall unloaded diameter of tire (m)

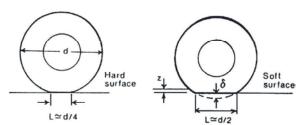


Fig. 1: Contact lengths of tires on hard and soft surfaces, adapted from McKyes [1]

Moreover, Wong [2] and Bekker [3] gave an approximate method for calculating contact length of tire as given below in equation 4:

$$L = 2(d\delta - \delta^2)^{0.5} \tag{4}$$

where:

 δ = Deflection of tire (m)

Tire contact length is a key parameter and many equations have been developed based on tire contact length to evaluate the tractive performance of radial-ply and bias-ply tires operating in cohesive-frictional soils. Gross traction, motion resistance, net traction and tractive efficiency are predicted as a function of soil strength, tire

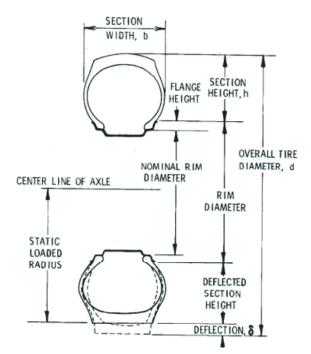


Fig. 2: Tire dimensions, adapted from Brixius [4]



Fig. 3: Tire contact length measurement apparatus

Table 1: Overall unloaded diameter of three radial-ply tires used in this study

Study	
Tire No.	Overall unloaded diameter d (mm)
1	578
2	582
3	605

load, tire slip, tire size, tire deflection and tire contact length [4]. Fig. 2 shows the tire dimensions (b, d and δ) used. The tire dimensions can be obtained from tire data book or by measuring the tire. The section width (b) is the first number in a tire size designation. The overall unloaded diameter (d) can be obtained from the tire data handbooks available from off-road tire manufacturers. The tire deflection (δ) on a hard surface is equal to d/2 minus the measured static loaded radius. The static loaded radius for the tire's rated load and inflation pressure is standard tire data from the tire data handbooks. It can also be obtained by measuring the tire [4, 5].

As contact length for a given tire size, inflation pressure, vertical load and rotational speed may significantly be different between radial-ply and bias-ply tires, this study was conducted to model contact length (L) of radial-ply tire based on overall unloaded diameter (d), inflation pressure (P), vertical load (W) and rotational speed (N) using a linear regression model.

MATERIALS AND METHODS

Tire Contact Length Test Apparatus: A tire contact length test apparatus was designed and constructed to measure contact length of tires with different sizes at diverse levels of inflation pressure, vertical load and rotational speed (Fig. 3).

Experimental Procedure: For this purpose, contact length of three radial-ply tires with different overall unloaded diameter were measured at three levels of inflation pressure, four levels of vertical load and six levels of rotational speed. The overall unloaded diameter of three radial-ply tires is given in Table 1. Results of contact length measurement for radial-ply tires No. 1, 2 and 3 are given in Tables 2, 3 and 4, respectively.

Regression Model: A typical four-variable linear regression model is shown in equation 5 [6-11]:

$$Y = C_0 + C_1 X_1 + C_2 X_2 + C_3 X_3 + C_4 X_4$$
(5)

				Contact length L (mm)			
verall unloaded diameter d (mm)	Inflation pressure P (psi)	Vertical load W (kg)	Rotational speed N (rev/min)		L ₂	L ₃	
78	30	100	0	121	121	120	
			600	115	115	11:	
			700	114	114	11-	
			800	113	113	11	
			900	112	112	11	
			1000	111	111	11	
		150	0	138	138	13	
			600	131	131	13	
			700	130	130	13	
			800	128	128	12	
			900	127	127	12	
			1000	126	126	12	
		200	0	148	148	14	
			600	141	141	14	
			700	140	140	14	
			800	139	139	13	
			900	138	138	13	
			1000	137	137	13	
		250	0	157	157	15	
			600	151	151	15	
			700	150	150	1:	
			800	149	149	14	
			900	148	148	14	
			1000	147	147	14	
	35	100	0	104	103	10	
			600	97	97	9′	
			700	96	96	96	
			800	95	95	95	
			900	94	94	94	
			1000	93	93	93	
		150	0	122	122	12	
			600	116	117	11	
			700	115	115	1	
			800	113	112	11	
			900	111	110	1	
			1000	109	109	10	
		200	0	139	139	13	
			600	135	135	13	
			700	134	134	13	
			800	133	133	13	
			900	132	132	13	
			1000	131	132	13	
		250	0	151	150	15	
			600	146	146	14	
			700	145	145	14	
			800	144	144	14	
			900	143	143	14	
			1000	142	142	14	

		Vertical load W (kg)		Contact length L (mm)			
Overall unloaded diameter d (mm)	Inflation pressure P (psi)		Rotational speed N (rev/min)	 L ₁	L ₂	L ₃	
	40	100	0	86	87	86	
			600	83	82	83	
			700	82	82	82	
			800	80	80	80	
			900	78	78	79	
			1000	77	77	76	
		150	0	104	104	105	
			600	99	99	100	
			700	98	97	97	
			800	96	95	95	
			900	93	94	93	
			1000	91	91	91	
		200	0	125	125	12:	
			600	119	119	119	
			700	118	117	11′	
			800	116	116	110	
			900	115	115	11:	
			1000	114	115	114	
		250	0	134	134	134	
			600	128	127	12	
			700	126	126	12	
			800	125	125	12:	
			900	124	124	124	
			1000	123	123	123	

Table 3: Overall unloaded diameter, inflation pressure, vertical loa	d, rotational speed and contact length (three replications) for radial-ply tire No. 2
	Contact length L (mm)

				Contact length L (mm)			
Overall unloaded diameter d (mm)	Inflation pressure P (psi)	Vertical load W (kg)	Rotational speed N (rev/min)	 L ₁	L ₂	L ₃	
582	30	100	0	110	110	110	
			600	104	104	103	
			700	102	102	101	
			800	100	100	99	
			900	99	99	99	
			1000	98	98	98	
		150	0	129	129	129	
			600	125	125	125	
			700	124	124	124	
	200		800	123	123	122	
			900	122	122	122	
			1000	121	121	120	
		200	0	151	151	151	
			600	148	148	147	
			700	147	147	146	
			800	147	147	146	
			900	146	146	145	
			1000	145	145	145	
		250	0	168	168	168	
			600	164	164	163	
			700	163	163	162	
			800	162	162	161	
			900	161	161	160	
			1000	160	160	160	

				Contact	length L (m	m)
verall unloaded diameter d (mm)	Inflation pressure P (psi)	Vertical load W (kg)	Rotational speed N (rev/min)	L ₁	L ₂	L ₃
	35	100	0	95	95	95
			600	90	90	89
			700	89	89	89
			800	87	87	87
			900	86	86	86
			1000	85	84	84
		150	0	114	114	1
			600	100	100	10
			700	98	98	9
			800	97	97	9
			900	96	96	9
			1000	95	95	9:
		200	0	130	130	13
			600	126	126	12
			700	125	125	12
			800	124	123	12
			900	123	122	12
			1000	121	121	12
		250	0	140	140	14
		230	600	137	137	1.
			700	136	136	1.
			800	135	135	1.
			900	135	135	1.
			1000	133	133	1
	40	100	0	87	87	8
			600	82	82	8
			700	81	81	80
			800	80	80	7
			900	79	79	7
			1000	78	78	7
		150	0	105	105	10
			600	99	99	9
			700	98	98	9
			800	97	97	9
			900	96	96	9
			1000	95	95	9
		200	0	117	117	1
		200	600	113	113	1
			700	112	112	1
			800	112	112	1
			900	110	110	1
			1000	109	109	10
		250	0			13
		230		132	132	
			600	126	126	12
			700	126	126	12
			800	125	125	12
			900	124	124	12

				Contact length L (mm)			
verall unloaded diameter d (mm)	Inflation pressure P (psi)	Vertical load W (kg)	Rotational speed N (rev/min)	 L ₁	L ₂	L	
05	30	100	0	99	99	99	
			600	93	93	92	
			700	92	92	9	
			800	91	91	9	
			900	90	90	8	
			1000	89	89	8	
		150	0	116	116	1	
			600	111	111	1	
			700	110	110	1	
			800	109	109	1	
			900	108	108]	
			1000	107	107]	
		200	0	130	130		
			600	127	127		
			700	126	126		
			800	125	125		
			900	124	124		
			1000	123	123		
		250	0	149	149		
			600	144	144		
			700	143	143		
			800	142	142		
			900	141	141		
			1000	140	140		
	35	100	0	80	80		
			600	76	76		
			700	75	75		
			800	74	74		
			900	73	73		
			1000	72	72		
		150	0	100	100		
			600	94	94		
			700	93	93		
			800	92	92		
			900	91	91		
			1000	90	90		
		200	0	118	118		
			600	113	113		
			700	112	112		
			800	111	111		
			900	110	110		
			1000	109	109		
		250	0	131	131		
			600	128	128		
			700	128	128		
			800	127	127		
			900	127	127		
			1000	126	126		

		Vertical load W (kg)	Rotational speed N (rev/min)	Contact length L (mm)			
Overall unloaded diameter d (mm)	Inflation pressure P (psi)				L ₂	L ₃	
	40	100	0	73	73	73	
			600	67	67	66	
			700	66	66	65	
			800	65	65	64	
			900	64	64	63	
			1000	63	62	63	
		150	0	87	87	8′	
			600	84	84	84	
			700	84	84	8	
			800	83	83	8	
			900	83	83	8	
			1000	82	82	8	
		200	0	98	98	9	
			600	95	95	9	
			700	94	94	9	
			800	94	94	9	
			900	93	93	9	
			1000	93	93	9	
		250	0	109	109	10	
			600	108	107	10	
			700	107	107	1	
			800	106	106	1	
			900	106	106	1	
			1000	105	105	1	

	p-value								
Model		Р	W	N	\mathbb{R}^2				
L = 552.1 - 0.656 d - 2.930 P + 0.320 W - 0.009 N	3.2E-222	0	0	2.18E-65	0.9711				

where:

Y = Dependent variable, for example contact length of radial-ply tire

 X_1, X_2, X_3, X_4 = Independent variables, for example overall unloaded diameter, inflation pressure, vertical load and rotational speed

 C_0, C_1, C_2, C_3, C_4 = Regression coefficients

To model contact length based on overall unloaded diameter, inflation pressure, vertical load and rotational speed, a four-variable linear regression model was suggested.

RESULTS AND DISCUSSION

In order to model contact length of radial-ply tire based on overall unloaded diameter, inflation pressure, vertical load and rotational speed, a four-variable linear regression model was suggested and all the data were subjected to regression analysis using the Microsoft Excel 2007. The four-variable linear regression model, p-value of independent variables and coefficient of determination (R^2) of the model are shown in Table 5. As it is shown in Table 5, this model has a high R^2 value at 0.9711, indicating good agreement of the experimental data. In addition, the p-value of independent variables (d, P, W and N) is as follows: 3.2E-222, 0, 0 and 2.18E-65, respectively. Thus, based on the statistical results, this model is initially accepted, which is given by equation 6:

L = 552.1 - 0.656 d - 2.930 P + 0.320 W - 0.009 N (6)

In this model, contact length of radial-ply tire can be predicted using a four-variable linear regression of overall unloaded diameter, inflation pressure, vertical load and rotational speed.

CONCLUSION

It can be concluded that the four-variable linear regression model L = 552.1 - 0.656 d - 2.930 P + 0.320 W - 0.009 N with R² = 0.9711 may be suggested to predict contact length of radial-ply tire based on overall unloaded diameter, inflation pressure, vertical load and rotational speed for a limited range of radial-ply tire sizes.

REFERENCES

- 1. McKyes, E., 1985. Soil Cutting and Tillage. Elsevier Science Publishing Company Inc., New York, USA.
- Wong, J.Y., 1978. Theory of Ground Vehicles. John Wiley and Sons, New York, USA.
- Bekker, M.G., 1985. The effect of tire tread in parametric analyses of tire-soil systems. NRCC Report No. 24146, National Research Council of Canada.
- Brixius, W.W., 1987. Traction prediction equations for bias ply tires. ASAE Paper No. 871622. St. Joseph, Mich.: ASAE.

- Goering, C.E., M.L. Stone, D.W. Smith and P.K. Turnquist, 2006. Off-Road Vehicle Engineering Principles. St. Joseph, Mich.: ASABE.
- Azadeh, S., M. Rashidi and M. Gholami, 2013. Modeling of bias-ply tire deflection based on tire dimensions, tire inflation pressure and vertical load on tire. Middle-East J. Sci. Res., 14(1): 117-121.
- Mousavi, M., M. Rashidi, I. Ranjbar, M. Solimani Garmroudi and M. Ghaebi, 2013. Modeling of bias-ply tire contact area based on tire dimensions, tire inflation pressure and vertical load on tire using linear regression models. Am-Euras. J. Agric. & Environ. Sci., 13(5): 627-632.
- Oroojloo, M., M. Rashidi and M. Gholami, 2013. Modeling of radial-ply tire contact area based on tire dimensions, tire inflation pressure and vertical load on tire. Middle-East J. Sci. Res., 17(7): 949-954.
- Sheikhi, M.A., M. Rashidi and M. Gholami, 2013. Modeling of radial-ply tire deflection based on tire dimensions, tire inflation pressure and vertical load on tire. Am-Euras. J. Agric. & Environ. Sci., 13(2): 222-226.